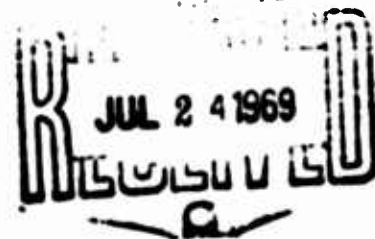


AD 690466

This document has been approved
for public release and since its
distribution is unlimited.

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED



HYDRONAUTICS, incorporated research in hydrodynamics

Research, consulting, and advanced engineering in the fields of NAVAL
and INDUSTRIAL HYDRODYNAMICS. Offices and Laboratory in the
Washington, D. C., area: Pindell School Road, Howard County, Laurel, Md.

Reproduced by the
CLEARINGHOUSE
for Federal Scientific & Technical
Information Springfield Va. 22151

HYDRONAUTICS, Incorporated

TECHNICAL REPORT 231-24

**EXPERIMENTS ON TURBULENT WAKES
IN A STABLE DENSITY-STRATIFIED
ENVIRONMENT**

By

**Walter P. M. van de Watering,
Marshall P. Tulin and Jin Wu**

February 1969

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

**Prepared Under
Office of Naval Research
Department of the Navy
Contract No. Nonr 3688(00)
NR 220-016**

TABLE OF CONTENTS

	Page
ABSTRACT.....	1
INTRODUCTION.....	1
INITIAL CONSIDERATIONS.....	3
EQUIPMENT AND EXPERIMENTAL TECHNIQUE.....	6
RESULTS.....	8
ANALYSIS AND DISCUSSION.....	9
CONCLUSIONS.....	17
REFERENCES.....	19

LIST OF FIGURES

- Figure 1 - Spiral Paddles, 10.16 cm and 5.08 cm in Diameter
- Figure 2 - Sample Pictures of Turbulent Mixed Region in Stratified Fluid
- Figure 3 - Typical History of a Turbulent Mixed Region in a Density Stratified Fluid
- Figure 4 - Dependence of Initial Conditions Upon Richardson Number
- Figure 5 - Correlation of Maximum Thickness, the Time Maximum Thickness is Reached and the Final Thickness with the Richardson Number
- Figure 6 - Graphical Determination of Final Thickness
- Figure 7 - Correlation of Maximum Thickness, Final Thickness and Degree of Mixing with the Richardson Number
- Figure 8 - Horizontal Spreading Before and After Onset of Collapse

NOTATION

a	Stratification strength, $-\frac{1}{\rho_0} \frac{\partial \rho}{\partial y}$
F, G	Functions
g	Gravitational acceleration
R_1	Richardson number
r_0	Radius of mixed region at $t = 0$ in uniform surroundings
t	Time after generation
t_{col}	Time the maximum thickness is reached
u_0	Velocity of advance of the boundary of a mixed region at $t = 0$ in a uniform medium
v_0	Vertical velocity of advance of the boundary of the mixed region in the vertical direction at $x = 0$ and $t = 0$ in a density-stratified medium
v	Vertical velocity of advance of the boundary of the mixed region in the vertical direction at $x = 0$ in a density-stratified medium
x	Abcissa of boundary of the mixed region at $y = 0$
x_0	Half the horizontal width at $t = 0$
y	Vertical ordinate of the boundary of the mixed region at $x = 0$ in a stratified medium
y_0	Vertical ordinate of the boundary of the mixed region at $x = 0$ and $t = 0$ in a stratified medium
y_{max}	Maximum vertical ordinate of the boundary of the mixed region at $x = 0$ and $t = t_{col}$; half the maximum thickness

HYDRONAUTICS, Incorporated

-iv-

y_f	Half the final thickness of mixed region
ϕ	Degree of mixing
ρ	Fluid density
ρ_o	Fluid density at elevation of center of mixed region
$\frac{\partial \rho}{\partial y}$	Density gradient
μ	Dynamic viscosity
D	Diameter of body
V	Velocity of body

ABSTRACT

In a laboratory experiment, turbulent mixed regions were generated in a linearly density-stratified fluid and their behavior was studied. Such regions may occur in nature in the atmosphere and in the ocean. Particularly during their early history, the shape of such regions is influenced by the interacting effects of turbulence and buoyancy, culminating in the occurrence of a maximum thickness and subsequent vertical collapse. A Richardson number (equivalent to the ratio of the characteristic turbulence time and the Vaisala period) was found satisfactorily to correlate the data obtained, together with those previously obtained by other investigators with self-propelled bodies. An estimate is made of the degree of mixing that takes place inside a turbulent mixed region during its growth in stably-stratified surroundings; the effectiveness of this mixing determines the ultimate thickness to which the mixing region collapses.

INTRODUCTION

Stable density stratifications commonly exist in the atmosphere as well as in the ocean, and mixed turbulent regions are created in these media in a number of ways, for example, mixed patches produced by over-turning internal waves or the remnants of chimney trails or thermals in the atmosphere. Also bodies traveling through such media produce a quite different turbulent wake behind them than in a homogeneous medium. The

present study is concerned with the time history of a slice of such a wake from its generation onward, which is closely equivalent to studying the change of wake shape with distance behind the body.

In homogeneous surroundings, a turbulent wake grows in size due to turbulent diffusion at the boundary, the rate of spreading being directly proportional to the turbulent intensity. Due to spreading and turbulence decay, the turbulent intensity and consequently the spreading rate continuously decrease with time. In a stratified fluid, turbulent diffusion produces a density distribution inside the turbulent wake different from that of the surrounding fluid. At the same time buoyancy forces interact with the turbulence causing changes in the latter, see Webster (1964), for example. As the turbulent intensity decreases and the stabilizing buoyancy forces increase with time, a condition is reached wherein turbulent diffusion in the vertical direction is completely suppressed. At this instant, the wake or mixed region has reached a maximum vertical thickness. If the fluid inside the region is completely mixed and non-turbulent, all the interior fluid will flow to the level of the center of the wake, and with time the thickness becomes thinner and thinner, as was shown by Wu (1969). With incomplete turbulent mixing, the fluid inside will not have a uniform density and only a partial vertical collapse occurs as was previously observed by Schooley and Stewart (1963) and by Kennedy, Stockhausen and Clark (1966).

Except for the final stage the history of a turbulent wake in a density-stratified medium is shown herein to be governed by the Richardson number, a dimensionless combination of the initial turbulent intensity (actually, the initial spreading velocity of the wake), the density stratification of the medium, gravity, and the initial wake radius. The interesting parameters such as maximum thickness, time necessary to reach this maximum, and final thickness, are all seen to depend upon the value of this Richardson number.

The data for the present study are taken from experiments carried out by van de Watering (1966). His experiments and previous experimental results are reanalyzed herein. The present analysis not only explains, but even enables a prediction of the changes in cross-sectional shape with time, which are experienced by a turbulent mixed region in any linearly density-stratified medium.

INITIAL CONSIDERATIONS

The present study is concerned with the history of the cross-sectional shape of a turbulent wake (having an initial radius r_0 and a spreading rate u_0 in a homogeneous medium of density ρ_0 and viscosity μ), produced by a body which can be characterized by a diameter D and which travels with a velocity V through a density-stratified medium of density ρ_0 at the height of the vehicle, of viscosity μ , and density gradient $\partial\rho/\partial y$, while the gravitational acceleration is g . Newton's law for a fluid particle of volume Q and density ρ_0 , which is $\Delta\rho$ heavier than its surrounding fluid, states that the gravitational force, acting on this particle, is:

$$\Delta \rho g Q = (\text{mass}) \times (\text{acc.}) = (\rho_0 Q) \times (\text{acc.}) \quad [1]$$

From [1] the acceleration, denoted by g_* , is equal to

$$\text{acc.} = g_* = \frac{\Delta \rho}{\rho_0} g$$

For a linearly density-stratified fluid this acceleration is:

$$\frac{d^2 y}{dt^2} = g_* = \frac{-y \frac{\partial \rho}{\partial y} g}{\rho_0} \quad [2]$$

where y is the vertical distance from the particle to its equilibrium position.

In the present context r_0 is chosen as the length scale in [2]:

$$g_* = \frac{-r_0 \frac{\partial \rho}{\partial y} g}{\rho_0} = r_0 a g$$

From [2] it can be derived that the expression $\sqrt{\frac{-1}{\rho_0} \frac{\partial \rho}{\partial y} g}$

is the frequency at which a displaced particle, if released, will oscillate around its equilibrium position in a linearly stratified fluid. It is known as the Vaisala-Brunt frequency. We will refer to it as $\sqrt{a g}$.

In stratified fluid the following parameters are of interest: the initial and maximum thickness, $2y_o$ and $2y_{\max}$, respectively; the initial wake vertical spreading rate, v_o ; the time to reach this maximum thickness, t_{col} , and the final wake thickness, $2y_f$. These dependent variables are a function of the previously listed independent variables:

$$(y_o, v_o, y_{\max}, t_{col}, y_f) = F(r_o, u_o, D, V, \mu, g_*, \rho_o)$$

Using Buckingham's π -theorem one obtains

$$\left(\frac{y_o}{r_o}, \frac{v_o}{u_o}, \frac{y_{\max}}{r_o}, \frac{u_o t_{col}}{r_o}, \frac{y_f}{r_o} \right) = G \left(\frac{r_o}{D}, \frac{u_o}{V}, \frac{r_o u_o \rho_o}{\mu}, \frac{u_o^2}{r_o g_*} \right)$$

The ratio's $\frac{r_o}{D}$ and $\frac{u_o}{V}$ may be determined either by direct measurement or by model tests in wind or water tunnels. The determination of these ratio's is beyond the scope of the present paper, and they are assumed to be known in the following. The third independent dimensionless number is the Reynolds number. Since the flow is always turbulent the Reynolds number does not play a role. The five dimensionless dependent variables are thus seen to be solely a function of the fourth independent dimensionless number, generally known as the densimetric Froude number. Because of the proportionality of velocity of advance of the turbulent front, u_o , and the turbulent intensity, $\sqrt{u'^2}$, we may also see this number as a Richardson number, defined in this particular application as:

$$R_1 = \frac{r_o \sqrt{ag}}{u_o}$$

For the above reasons we may thus expect, that the five dimensionless parameters of interest will vary only if the Richardson number is varied. The Richardson number has been used before to scale flows in which turbulence and gravity forces are interacting (see e.g. Townsend, 1958, or Defant, 1961). It may also be thought of as the ratio of a characteristic turbulence time, r_o/u_o to a characteristic stratification time, $1/\sqrt{ag}$.

Through multiplication of two dimensionless numbers one obtains $t_{col} \sqrt{ag}$, which is to be preferred above $t_{col} u_o/r_o$ to non-dimensionalize the time it takes to reach the maximum vertical thickness.

Next let us see how the laboratory experiments prove that indeed the pertinent parameters associated with turbulent wake growth and collapse only depend upon the value of the Richardson number.

EQUIPMENT AND EXPERIMENTAL TECHNIQUE

The spatial behavior of a turbulent wake in a density-stratified fluid is believed closely equivalent to the time history of a thin slice of such a wake, considered as two-dimensional. With this analogy in mind we designed the experimental equipment and technique.

The experiments were carried out in a transparent lucite tank, 121 x 109 x 31.5 cm, in which a linear density stratification was obtained by mixing increasing amounts of sodium chloride in water and introducing these mixtures into the tank in layers through a diffusor placed on the bottom of the tank. The layers were 2.54 cm thick and alternately colored with red dye. In this way 24 layers were brought into the tank which formed initially a stepped density distribution. Overnight a linear density gradient was obtained through molecular diffusion, but the dye remained in discrete layers because of its relatively low diffusivity.

At mid-depth of this linearly density-stratified fluid, a spiral paddle was supported across the tank by a 0.8 cm I.D. brass tube and rotated forward and back by means of a pendulum type of arrangement at the back of the tank. Four rows of holes were drilled along this tube. Just prior to a test, a rod, heavily painted with a blue dye which rapidly dissolves in water, was inserted in the perforated center tube. The blue dye was used to facilitate visualization of the turbulent mixed region. The above-described technique to generate a turbulent mixed region was first used by Wu in 1965. Two spiral paddles were used in these experiments; one was 5.08 cm, the other 10.16 cm in diameter (see Figure 1). With the 5.08 cm paddle, two different pendulums were used so as to vary the turbulent mixing characteristics.

The life of the mixed region was photographed with a 16 mm movie camera. Zero time was taken at the instant the paddle motion stopped. Data were taken from tracings of projected frames of the movie film (see Figure 2).

If desired, more information pertaining to the experimental technique and apparatus can be obtained from the original data report by van de Watering (1966).

RESULTS

With the three combinations of paddles and pendulum, tests in pure water were carried out first. The cross-section of the mixed region during these tests remained more or less circular. From tracings, the averaged (root-mean-square) radius was determined and plotted versus time. The initial velocity of advance of the turbulent front in pure water, u_0 , together with the initial averaged radius of the turbulent region r_0 , are given in Table 1.

In density-stratified surroundings, the shape of the mixed region changes continuously. Just after generation, the cross-section is already non-circular and the density inside the mixed region is different from its surrounding medium, causing stabilizing gravitational forces to counteract turbulence. Webster (1964) and others clearly show that the vertical scale of turbulence is reduced. With increasing time the cross-section becomes more ellipse-like and eventually reaches a maximum thickness, after which a vertical collapse takes place to a finite

thickness, $2y_f$. A series of sample pictures is presented in Figure 2, in which the above-mentioned characteristics are clearly visible. For a typical time history see also Figure 3.

Since one of the primary aims of the present study was to relate turbulent mixing and density gradient with the characteristics of the mixed region, most attention was focused on the change with time of the vertical ordinate of the boundary of the mixed region at the center of the wake, since it is this thickness which is affected most by the interplay of turbulence and gravity. For several runs the horizontal extent of the mixed region was also analyzed in order to obtain information on the rate of collapse. For all tests, the actual measured values for half the maximum thickness (y_{\max}), the time it took to reach this maximum (t_{col}) and half the final thickness (y_f) are given in Table 1.

ANALYSIS AND DISCUSSION

In a stably stratified fluid, the vertical ordinate and velocity of the boundary of the mixed region, both taken at the center of the wake and given the symbols y and v respectively, are affected by the interaction of turbulence and density stratification and by the length scale. The experiments indicate that this interaction is already effective during the generation stage. The data show, see Table 1, that at zero time, y_0 , and v_0 are in almost all tests smaller than their corresponding values in pure water, r_0 and u_0 . In Figure 4 the

dimensionless initial vertical ordinate and velocity are plotted versus the Richardson number. We have included the data points from the two studies with self-propelled bodies, the experiments by Schooley and Stewart (1963) and by Kennedy, Stockhausen and Clark (1966). From the former study, the values for r_0 and u_0 were obtained from the original movie film of these authors, i.e., from tracings of projected frames of their film of the two runs in pure water. At this point, it may be mentioned that in their analysis, a small error was made in the calculations of the density gradient. The corrected value for \sqrt{ag} is 2.19 sec^{-1} while u_0 was found to be 5.87 cm/sec and r_0 equal to 0.568 cm . For the experiment carried out by Kennedy, et al, the correct Vaisala-Brunt frequency is: $\sqrt{ag} = 0.25 \text{ sec}^{-1}$. The values for u_0 and r_0 were obtained from the curve of the horizontal width of the wake, which is not significantly affected by gravitational effects until collapse starts. The values obtained from these studies are tabulated in Table 1.

The velocity seems much more affected by the interaction than the thickness, see Figure 4. The scatter of the data does not justify a definite relation, but the tendencies are clear. For increasing Richardson numbers, (corresponding to a large stratification), both y_0/r_0 and v_0/u_0 tend to be reduced, while for small Richardson numbers (turbulence is large compared to stratification), in the range from 0 to 1, there is no significant effect. In the ocean, R_1 may vary from about 0.06 to 0.9

and we may thus safely say that in this range the effect of stratification upon initial conditions is negligible for all practical applications.

During the growth stage the buoyancy forces increase while the turbulence decreases in intensity. The increasing dominance of buoyancy culminates at some time after generation, t_{col} , in a maximum wake thickness ($=2y_{max}$). The maximum thickness, y_{max}/r_o , where r_o is the radius of the circular mixed region in uniform surroundings at time zero, is plotted in Figure 5a. In all laboratory experiments on turbulent wake collapse, the maximum thickness can be observed and measured rather accurately. Due to the nature of the variation of thickness with time it is much more difficult accurately to determine the time at which this maximum occurs. Therefore, we may expect more scatter in the data of t_{col} as compared to those of y_{max} . The data are presented in Figure 5b. It is not possible accurately to determine the time at which collapse started from the experimental results as given by Kennedy and his co-workers. Therefore, the possible range of t_{col} \sqrt{ag} is indicated.

During the growth stage, the turbulent mixing inside the wake will produce therein a density gradient less pronounced than that of the surrounding fluid. After the wake grows to its maximum thickness, the fluid particles within seek their equilibrium level under the action of hydrostatic pressures. The mixed region decreases in thickness and spreads rapidly horizontally. This phenomenon is known as wake collapse (Schooley

and Stewart, 1963 and Schooley, 1967). If the mixed region is non-turbulent and fully mixed, a long thin wedge will be formed, which becomes thinner with increasing time; such well mixed regions have been observed and studied by Wu (1969). Inside the usual turbulent mixed region in a stratified fluid, turbulent diffusion does not succeed in mixing completely the wake contents, and it is for this reason that there exists an effective density distribution within the wake at the time when the maximum thickness is reached. This density distribution inside the mixed region should again depend only upon the Richardson number.

Wake collapse is driven by the hydrostatic pressure resulting from the differences between the exterior (ambient) and interior density gradients. The interior gradient is continually increased as a result of the vertical shrinking of the wake. The mixed region thus reaches a final thickness, $(2y_f)$, corresponding to which these density gradients are of equal value. The measured values of y_f are given in Table 1 and plotted dimensionlessly in Figure 5c.

The trend of the data, shown in Figures 5a, 5b and 5c, is readily explained. A turbulent mixed region in homogeneous fluid ($R_1 = 0$) will continue to grow indefinitely in size and y_{max} , t_{col} and y_f are unbounded at this limit. On the other hand the non-turbulent mixed region (Wu, 1969) in density-stratified fluid ($u_0 = 0$ and $R_1 \rightarrow \infty$) is the other limit for which we know that there is no growth, i.e., $t_{col} = 0$, while y_f approaches zero. In between these limits the data show a

gradual increase in the value of the parameters as the Richardson number decreases, i.e. as the wake becomes relatively more turbulent. The opposite case, i.e. decreasing maximum thickness, time to reach maximum thickness, and final thickness, is observed when the density gradient or R_1 is increased. This interpretation also explains why it was observed that with the larger paddle (larger R_1) the turbulent mixed region did not seem to have much strength i.e. the maximum thickness was small compared with the initial diameter in a homogeneous medium.

In the past, the time t_{col} has generally been considered as solely dependent upon the density gradient (see for instance Schooley, 1967 and 1968), but the present analysis shows that it is the Richardson number that actually governs the value of $t_{col} \sqrt{ag}$.

Let us suppose as an approximation that at $t = t_{col}$ a linear density gradient $(\partial\rho/\partial y)_{internal}$ exists inside the mixed region, see Figure 6. The difference in density of the fluid at the top of the wake, (1) in Figure 6, compared to fluid in the center (2), is:

$$\rho_1 - \rho_0 = y_{max} \cdot (\partial\rho/\partial y)_{internal}$$

If we assume that no further mixing takes place after t_{col} , then finally:

$$y_{max} (\partial\rho/\partial y)_{internal} = y_f (\partial\rho/\partial y)_{external}$$

So that,

$$\frac{y_f}{y_{\max}} = \frac{\left(\frac{\partial \rho}{\partial y}\right)_{\text{internal at } t_{\text{col}}}}{\left(\frac{\partial \rho}{\partial y}\right)_{\text{external}}} \quad [3]$$

The right hand side of this expression is a measure for the degree of mixing, ϕ , which takes place during growth and which we define as:

$$\phi = \left[1 - \frac{\left(\frac{\partial \rho}{\partial y}\right)_{\text{internal at } t_{\text{col}}}}{\left(\frac{\partial \rho}{\partial y}\right)_{\text{external}}} \right] \quad [4]$$

expressed in percent. Combining [3] and [4], the degree of mixing is:

$$\phi = \left[1 - \frac{y_f}{y_{\max}} \right] \times 100 \quad [5]$$

In Figure 7 the values of y_f/y_{\max} and ϕ are plotted versus the Richardson number. Increasing the density gradient (i.e., increasing the value of the Richardson number) will result in less mixing and from Figure 7 it is seen that indeed the degree of mixing decreases with increasing Richardson number. Mixing is generally poor: the degree of mixing, ϕ , is about 40 percent at the smallest Richardson numbers and decreases if R_1 increases.

As far as horizontal wake spreading is concerned, it should be realized first that a turbulent wake expands naturally unless opposed, as by hydrostatic pressures. While stratification acts against expansion in the vertical direction, it actually enhances the horizontal expansion. Initially the horizontal expansion is dominated by turbulence and the effect of stratification is small. Consequently the horizontal expansion until collapse sets in, will be close to the pure water case. However, once, the maximum vertical thickness is reached, the wake collapses vertically and the fluid spreads out horizontally under the action of hydrostatic pressures. We may thus not be surprised to observe a sudden surge in horizontal expansion some short time after collapse sets in. At this time gravitational forces start to play a completely dominant role. For several runs the horizontal spreading is plotted dimensionlessly in Figure 8. A distinct discontinuity in the $x-t$ curves is noticeable and it occurs in each case a short time after the maximum thickness is reached.

In experiments with a non-turbulent mixed region, the area of mixed fluid remains constant throughout a test. In a turbulent mixed region, an increase in cross-sectional area with time due to turbulent entrainment is observed. In stratified fluid, we observed turbulent entrainment even after the maximum thickness was reached. A continuous increase in area was measured, although the rate of area increase decreased gradually with time.

The vertical collapse of the mixed region generated internal waves in the surrounding fluid due to displacement of mixed fluid by the ambient medium. In a turbulent mixed region, even after the onset of collapse, there is still turbulence, albeit that the motion is dominated by gravitational effects. This turbulence, which tends to expand the mixed region, tends to soften wake collapse. The net result is to increase the characteristic time of wake collapse over that observed in the case of the collapse of a non-turbulent mixed region. This time is further increased because of the density gradient existing within the wake. Furthermore, in the turbulent case the mixed region typically collapses to a final thickness which is a large fraction of the maximum thickness. This is shown in Figure 7. The punch action of the impulsive collapse is therefore not only slower in time, but also of a smaller amplitude. Collapsing turbulent mixed regions are consequently less effective generators of internal waves than non-turbulent completely mixed regions. All of these effects were observed in the present experiments.

Two other interesting features were also observed which seem to be characteristic for a collapsing turbulent mixed region. After reaching its maximum thickness, mixed fluid spreads out horizontally and the upper and lower wake boundaries become more or less flat; this was particularly clear near and after the time when the final thickness was reached. Simultaneously, "finger-like" puffs of mixed fluid began protruding horizontally away from the bulk of the wake. Presumably these phenomena are due to the action in the large turbulent eddies, which are suppressed and flattened by the stabilizing buoyancy forces.

CONCLUSIONS

A turbulent mixed region in a density-stratified fluid undergoes changes as a result of the interplay between turbulence and stabilizing buoyancy forces. Some time after generation the mixed region reaches a maximum vertical thickness, after which vertical collapse and horizontal spreading take place. Due to incomplete mixing, the density of the fluid inside the region is not uniform, and, consequently, the mixed fluid reaches an equilibrium shape with a finite vertical thickness. Based on the present experimental results, obtained from tests using paddle mixers as generators of turbulent mixed regions, and on other available data from previous studies by other investigators, the maximum thickness, the time it takes to reach this maximum, and the final thickness, are shown to depend upon the ratio of the characteristic turbulence time to the Vaisala-Brunt period.

This ratio is in the form of a Richardson number. The present correlation provides an explanation for the higher values of the maximum thickness and the time to reach this maximum, as obtained by other investigators with self-propelled bodies under conditions of relatively small Richardson numbers.

A rough picture of turbulent wake collapse is presented with which, together with a knowledge of the ratio of final to maximum thickness (which can be estimated from the present correlation), the degree of mixing inside the wake can be estimated. Mixing is generally poor, in the order of 10 to 40 percent (in a completely mixed fluid the mixing is 100 percent).

The collapse of a turbulent mixed region in a density-stratified medium generates less pronounced internal waves in comparison with a non-turbulent, completely mixed region.

The present experiments revealed the formation of a flat top and bottom of the mixed region and of "finger-like" puffs of mixed fluid spreading horizontally outward.

REFERENCES

- Defant, A., 1961, Physical Oceanography, Pergamon Press.
- Kennedy, J. F., Stockhausen, P. J., and Clark, C. B., 1966, Three-Dimensional Momentumless Wakes in Density-Stratified Liquids, M.I.T., Hydrodynamics Laboratory Report No. 93, p. 80.
- Schooley, A. H., 1968, Wake Collapse in Stratified Fluid: Experimental Exploration of Scaling Characteristics, Science, Vol. 160, pp. 763-764.
- Schooley, A. H. and Stewart, R. W., 1963, Experiments with a Self-Propelled Body Submerged in a Fluid with a Vertical Density Gradient, J. Fluid Mech., 15, pp. 83-96.
- Townsend, A. A., 1958, Turbulent Flow in a Stably Stratified Atmosphere, J. Fluid Mech., 3, Part 4.
- van de Watering, W.P.M., 1966, The Growth of a Turbulent Wake in a Density-Stratified Fluid, HYDRONAUTICS, Incorporated Technical Report 231-12.
- Webster, C.A.G., 1964, An Experimental Study of Turbulence in a Density-Stratified Shear Flow, J. Fluid Mech., 19, pp. 221-265.
- Wu, Jin, 1969, Mixed Region Collapse with Internal Wave Generation in A Density-Stratified Medium, J. Fluid Mech., Vol. 35, No. 3, pp. 531-544.
- Wu, Jin, 1965, Experiments on Free Turbulence in Visco-Elastic Fluids, HYDRONAUTICS, Incorporated Technical Report 353-1.

TABLE 1

Investigators	r_o, y_o cm	u_o, v_o cm/sec	\sqrt{ag} sec ⁻¹	$r_o \sqrt{ag}$ u_o	t_{col} sec	$t_{col} \sqrt{ag}$	y_{max} cm	y_{max}/r_o	y_{final} cm	y_{final} r_o
van de Watering 1966	4.83	0.890	0.000	0.00	∞	1.33	∞	∞	∞	∞
	4.64	0.890	0.254	1.34	5.25	1.48	7.26	1.51	5.36	1.110
	3.96	0.763	0.296	1.56	5.00	1.21	6.03	1.25	5.03	1.041
	4.35	0.813	0.296	1.56	4.10	1.35	6.33	1.31	5.61	1.162
	3.81	0.701	0.415	2.19	3.25	1.35	5.36	1.11	4.34	0.898
	3.91	0.767	0.415	2.19	3.25	1.35	5.74	1.19	4.35	0.900
	4.08	0.620	0.585	3.09	2.40	1.40	5.10	1.06	--	--
	4.07	0.432	0.820	4.33	1.50	1.23	4.59	0.95	3.74	0.774
	4.14	0.610	0.810	4.27	1.30	1.05	4.83	1.00	4.02	0.832
	4.50	1.170	0.000	0.00	∞	1.12	∞	∞	∞	∞
	4.06	0.915	0.408	1.56	2.75	1.12	5.56	1.24	4.22	0.937
	3.73	0.889	0.408	1.57	2.75	1.12	5.62	1.25	3.99	0.886
	4.14	0.871	0.593	2.28	1.50	0.89	5.38	1.20	4.50	1.000
	4.22	0.686	0.833	3.21	1.50	1.25	5.08	1.13	4.22	0.937
	7.81	1.740	0.000	0.00	∞	1.05	∞	∞	∞	∞
	8.18	0.661	0.420	2.06	2.52	1.05	9.35	1.20	8.00	1.025
	7.11	0.548	0.418	1.89	1.75	0.73	8.15	1.04	6.88	0.881
	7.52	0.787	0.814	3.69	1.30	1.07	8.18	1.04	--	--
	6.30	1.068	1.165	5.21	1.10	1.28	6.91	0.88	6.00	0.769
	6.71	0.839	1.181	5.29	1.00	1.18	7.42	0.95	6.84	0.876
Kennedy, Clark and Stockhausen 1966	7.78	4.14	0.00	0.00	∞	1.63-3.25	∞	∞	∞	∞
	7.78	4.14	0.25	0.47	6.5-13	17.17	17.17	2.12	11.88	1.516
Schooley and Stewart 1963	0.568	5.87	0.00	0.000	∞	2.12	∞	∞	∞	∞
	0.568	5.87	2.19	0.212	0.97		2.375	4.18	1.5	2.64

HYDRONAUTICS, INCORPORATED

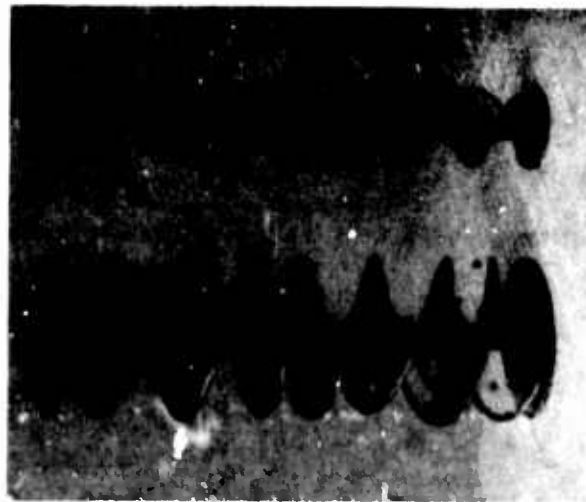


FIGURE 1 - SPIRAL PADDLES; 10.16 cm AND 5.08 cm IN DIAMETER

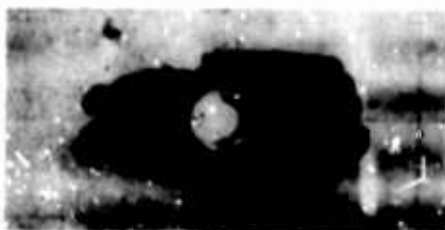


$t\sqrt{g\beta} = 0$
(JUST AFTER GENERATION)



$t\sqrt{g\beta} = 1.33$
(MAXIMUM THICKNESS)

$$\sqrt{g\beta} = 0.254 \text{ sec}^{-1}$$



$t\sqrt{g\beta} = 4.10$



$t\sqrt{g\beta} = 7.00$

FIGURE 2 - SAMPLE PICTURES OF TURBULENT MIXED REGION IN STRATIFIED FLUID

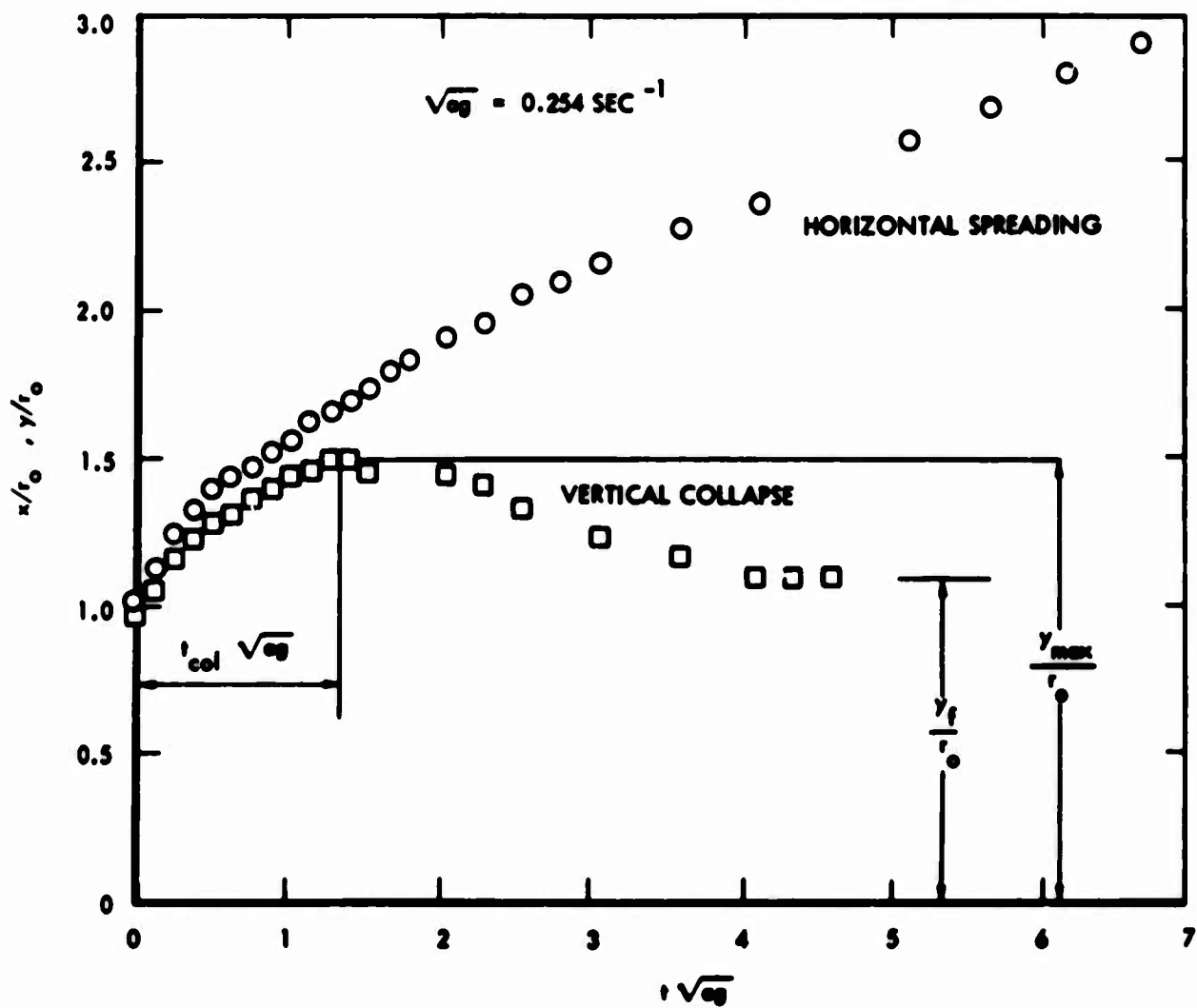


FIGURE 3 - TYPICAL HISTORY OF A TURBULENT MIXED REGION IN A DENSITY - STRATIFIED MEDIUM.

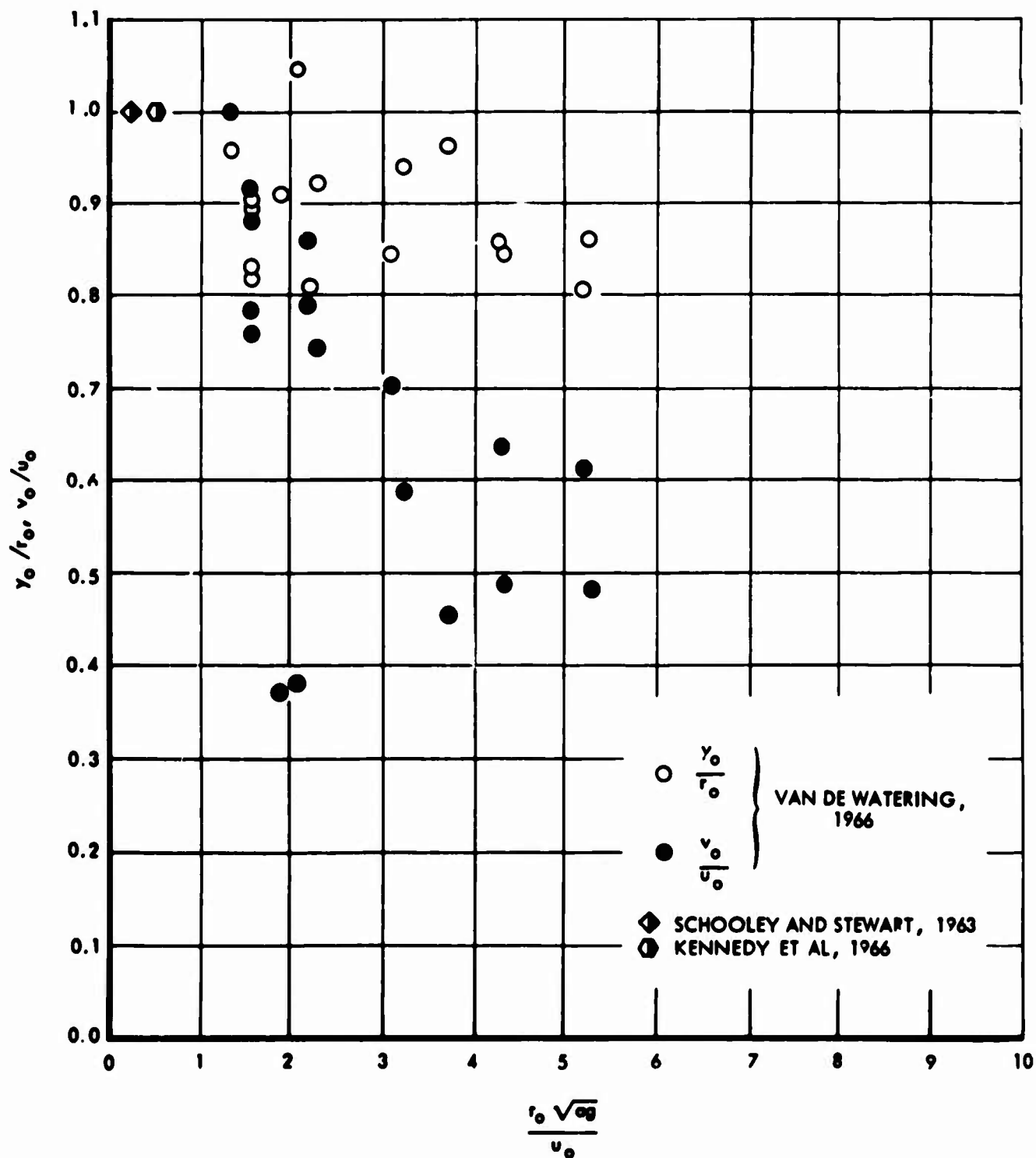


FIGURE 4 - DEPENDENCE OF INITIAL CONDITIONS UPON RICHARDSON NUMBER.

HYDRONAUTICS, INCORPORATED

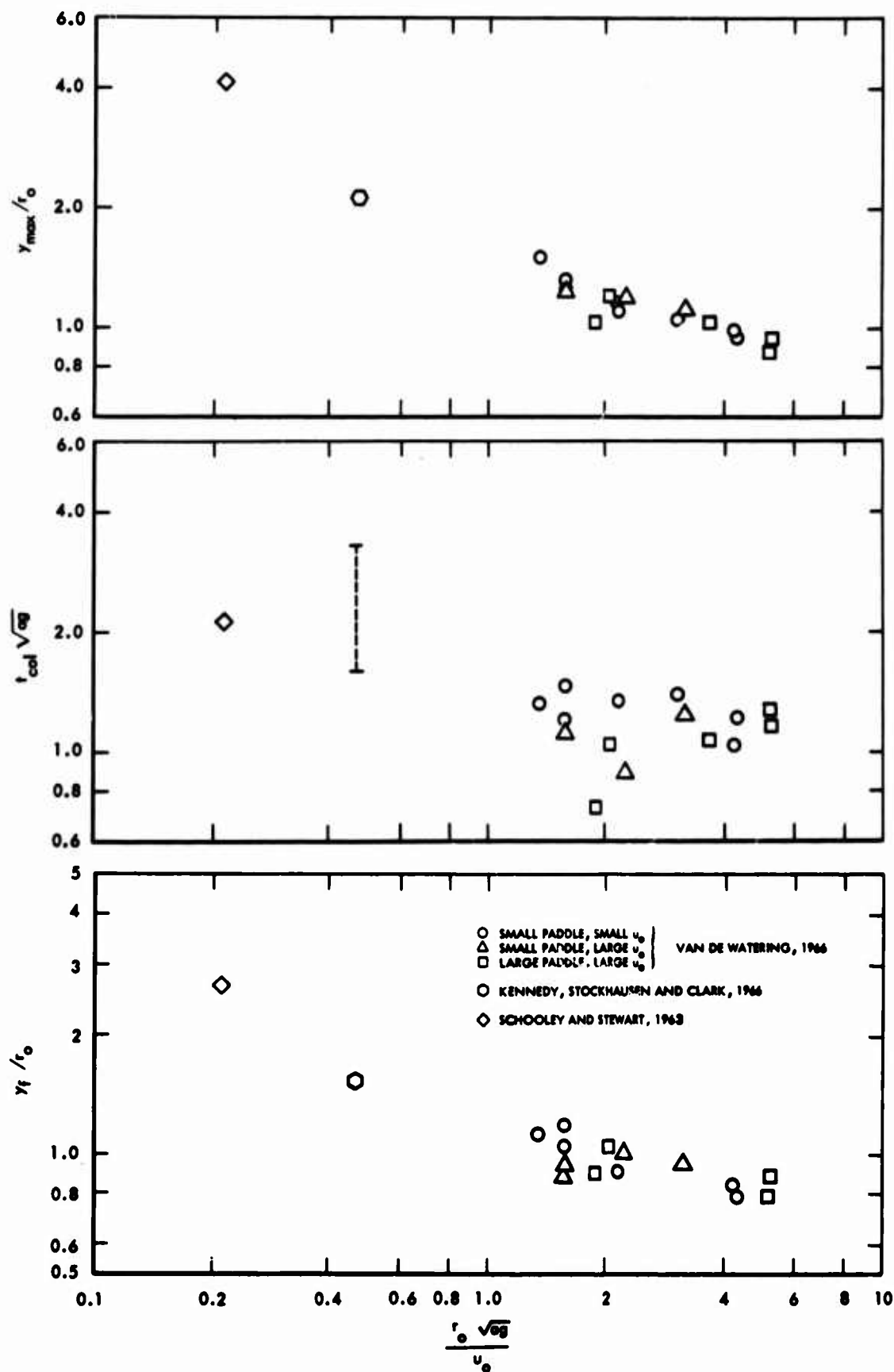


FIGURE 5 - CORRELATION OF MAXIMUM THICKNESS, THE TIME MAXIMUM THICKNESS IS REACHED AND THE FINAL THICKNESS WITH THE RICHARDSON NUMBER.

HYDRONAUTICS, INCORPORATED

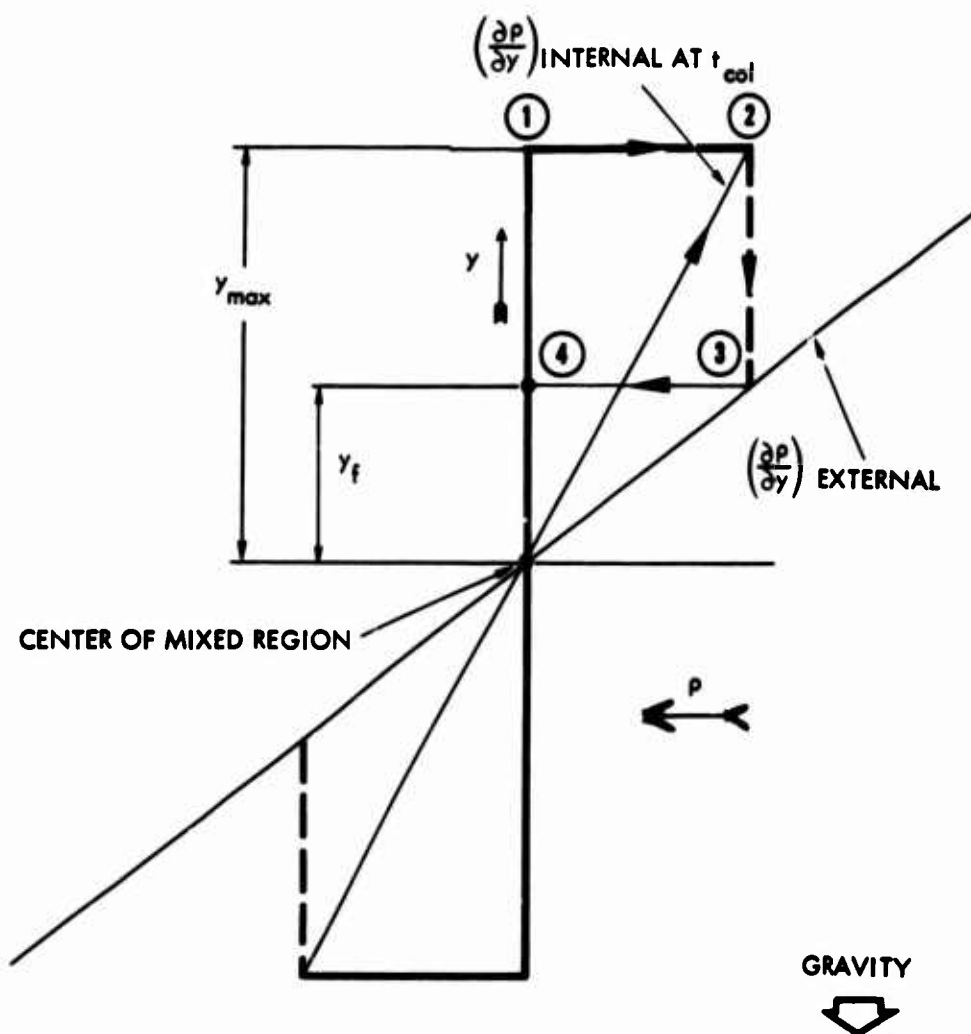


FIGURE 6 - GRAPHICAL DETERMINATION OF FINAL THICKNESS

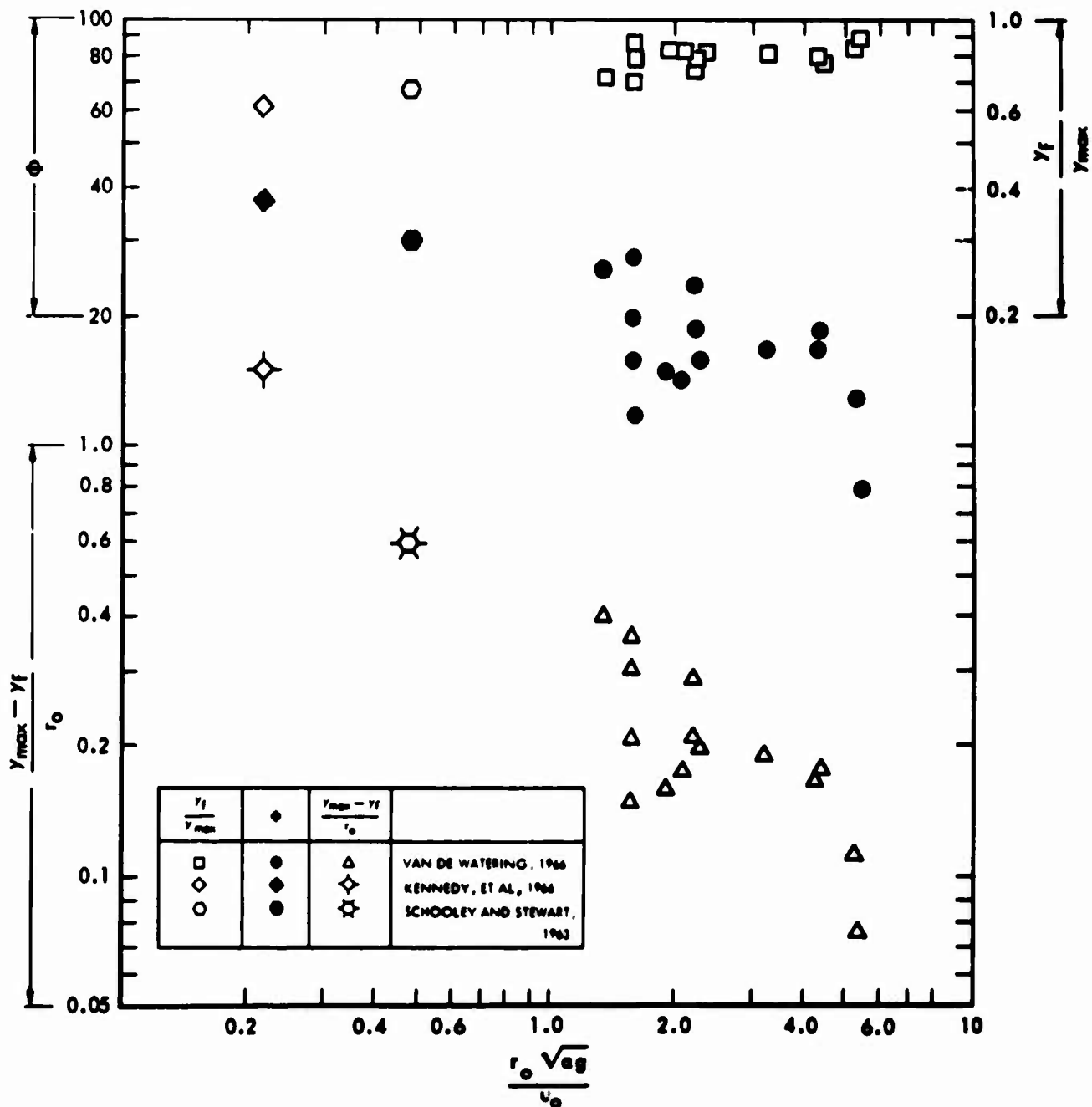


FIGURE 7 - CORRELATION OF MAXIMUM THICKNESS, FINAL THICKNESS AND DEGREE OF MIXING WITH THE RICHARDSON NUMBER.

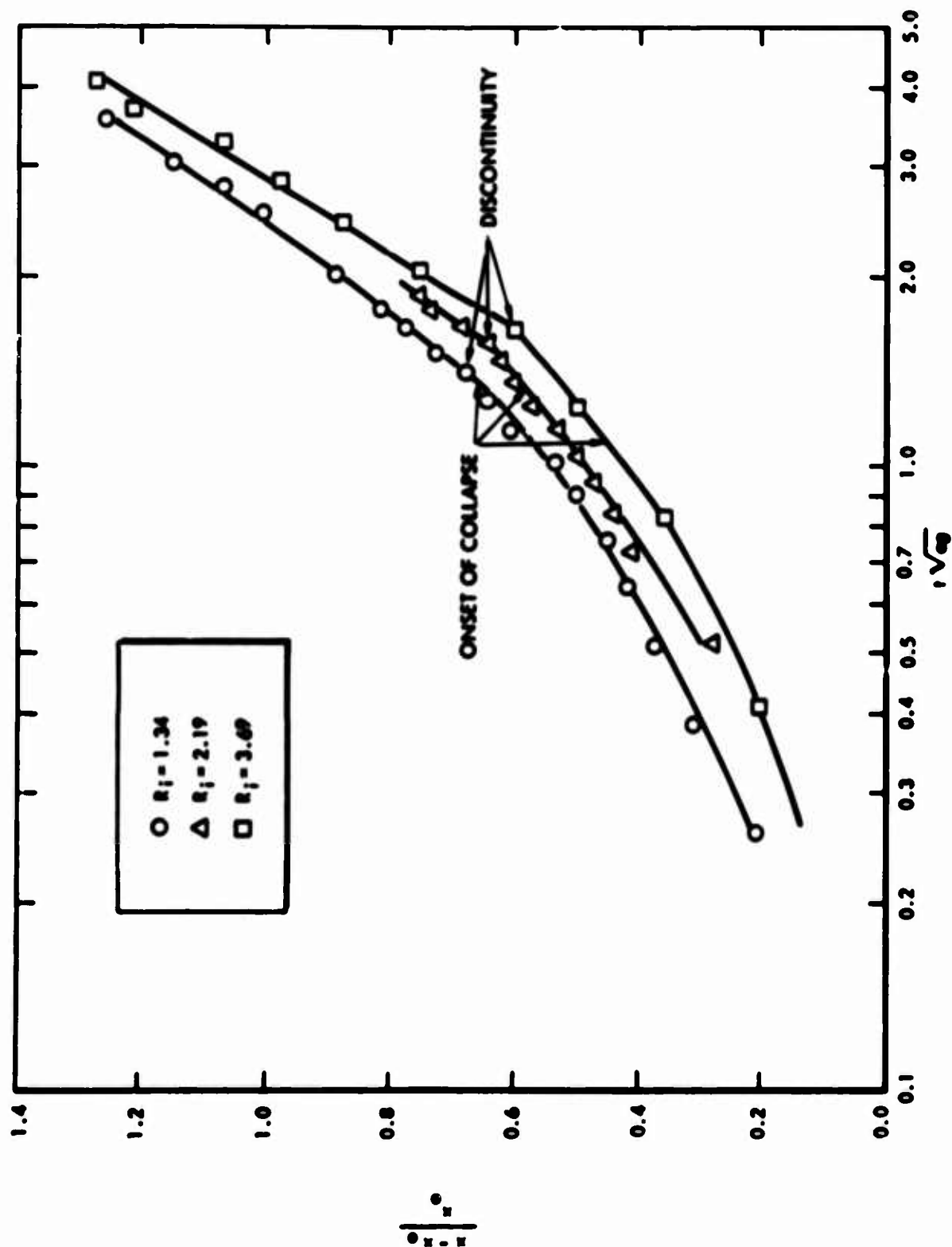


FIGURE 8 - HORIZONTAL SPREADING BEFORE AND AFTER ONSET OF COLLAPSE

UNCLASSIFIED

Security Classification

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) HYDRONAUTICS, Incorporated Pindell School Road, Howard County, Laurel, Maryland		2a. REPORT SECURITY CLASSIFICATION Unclassified	
3. REPORT TITLE EXPERIMENTS ON TURBULENT WAKES IN A STABLE DENSITY-STRATIFIED ENVIRONMENT		2b. GROUP	
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Technical Report			
5. AUTHOR(S) (Last name, first name, initial) van de Watering, Walter P. M. Tulin, Marshall P., and Wu, Jin			
6. REPORT DATE February 1969	7a. TOTAL NO. OF PAGES 30	7b. NO. OF REFS 9	
8a. CONTRACT OR GRANT NO. Nonr 3688(00), NR 220-16 b. PROJECT NO. c. d.		9a. ORIGINATOR'S REPORT NUMBER(S) Technical Report 231-24 9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
10. AVAILABILITY/LIMITATION NOTICES Distribution of this document is unlimited			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Office of Naval Research Department of the Navy	
13. ABSTRACT In a laboratory experiment, turbulent mixed regions were generated in a linearly density-stratified fluid and their behavior was studied. Such regions may occur in nature in the atmosphere and in the ocean. Particularly during their early history, the shape of such regions is influenced by the interacting effects of turbulence and buoyancy, culminating in the occurrence of a maximum thickness and subsequent vertical collapse. A Richardson number (equivalent to the ratio of the characteristic turbulence time and the Vaisala period) was found satisfactorily to correlate the data obtained, together with those previously obtained by other investigators with self-propelled bodies. An estimate is made of the degree of mixing that takes place inside a turbulent mixed region during its growth in stably-stratified surroundings; the effectiveness of this mixing determines the ultimate thickness to which the mixing region collapses.			

DD FORM 1473
1 JAN 64

UNCLASSIFIED

Security Classification

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Turbulent Wake in Stratified Fluid						
Wake Growth						
Wake Collapse						
Turbulence Suppression						
Stratified Fluid						
Continuous Density Gradient						
Turbulence						
Richardson Number						
Turbulent Mixing						
Internal Waves						

INSTRUCTIONS

1. ORIGINATING ACTIVITY: Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. REPORT SECURITY CLASSIFICATION: Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. GROUP: Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. REPORT TITLE: Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. DESCRIPTIVE NOTES: If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. AUTHOR(S): Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. REPORT DATE: Enter the date of the report as day, month, year, or month, year. If more than one date appears on the report, use date of publication.

7a. TOTAL NUMBER OF PAGES: The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. NUMBER OF REFERENCES: Enter the total number of references cited in the report.

8a. CONTRACT OR GRANT NUMBER: If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. PROJECT NUMBER: Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. ORIGINATOR'S REPORT NUMBER(S): Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. OTHER REPORT NUMBER(S): If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

10. AVAILABILITY/LIMITATION NOTICES: Enter any limitations on further dissemination of the report, other than those

imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through _____."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through _____."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through _____."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. SUPPLEMENTARY NOTES: Use for additional explanatory notes.

12. SPONSORING MILITARY ACTIVITY: Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

13. ABSTRACT: Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. KEY WORDS: Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, roles, and weights is optional.